

Non-stationary stochastic dynamics analysis of structural systems equipped with fractional viscoelastic device

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1. Introduction

Viscoelastic materials are commonly used for vibration mitigation. The viscoelastic behaviour is defined by the Creep test, providing the Creep function. Starting from Nutting experiments (1921) [1] the creep function, $C(t)$, is

$$C(t) = t^\beta / E_\beta \Gamma(\beta+1); \quad 0 \leq \beta \leq 1 \quad (1)$$

where $C(\beta)$, β are found by best fitting procedure and $\Gamma(\cdot)$ is the Gamma function. By using the Boltzmann superposition principle for a power law creep function the fractional constitutive arise. Then, inserting a viscoelastic device into a structural system, a second order derivative, a fractional operator and elastic term appear. In this presentation the stochastic analysis for a non-stationary white noise input is discussed in time domain by using Grünwald-Letnikov integration scheme.

2. Results and Discussion

For a viscoelastic device with a creep function as in eq. (1), the Boltzmann superposition principle gives

$$\varepsilon(t) = \frac{1}{E(\beta)\Gamma(1+\beta)} \int_0^t (t-\tau)^\beta \dot{\sigma}(\tau) d\tau = \frac{1}{E_\beta \Gamma(\beta)} \int_0^t (t-\tau)^{\beta-1} \sigma(\tau) d\tau \quad (2)$$

The last equality in eq. (2) is proportional to the Riemann Liouville fractional integral, ${}_0 I_t^\beta$. The constitutive laws are, for quiescent system ($t \leq 0$)

$$\varepsilon(t) = \frac{1}{E_\beta} ({}_0 I_t^\beta \sigma)(t); \quad \sigma(t) = E_\beta ({}_0^c D_t \varepsilon)(t) \quad (3.a,b)$$

where ${}_0^c D_t^\beta$ in eq. (4.b) is the Caputo's fractional derivative. Then, for a structural system equipped with a viscoelastic device we may write:

$$\ddot{X} + 2\zeta_\beta \omega_0 ({}^c D_t^\beta X)(t) + \omega_0^2 x = \Psi^{\frac{1}{2}}(t)W(t); \Psi(t) > 0 \quad (4)$$

where ζ_β is the (anomalous) dissipation factor, ω_0 is the natural frequency, $\Psi(t)$ is a deterministic modulating function and $W(t)$ is characterized by the correlation function $R_w(\tau) = E[W(t)W(t+\tau)] = q\delta(\tau)$, being q the strength of white noise. The operators of derivatives and integrals may be inverted to obtain

$$X + 2\zeta_\beta \omega_0 ({}_0 I_t^{2-\beta} x)(t) + \omega_0^2 ({}_0 I_t^2 x)(t) = {}_0 I_t^2 \left(\Psi^{\frac{1}{2}}(t)W(t) \right) \quad (5)$$

that, by using the Grünwald-Letnikov integration scheme [2] we get

$$\mathbf{A}_n \mathbf{X}_n = \mathbf{B}_n \mathbf{W}_n \quad (6)$$

where $\mathbf{X}_n, \mathbf{W}_n$ are n -vectors whose j -th component are $X(t_j)$ and $W(t_j) =$

$(q\Psi(t_j)/\Delta t)^{1/2} N_j$, respectively. Moreover $t_j - t_{j-1} = \Delta t$; N_j are realizations of standard normal random variables with $E[N_i N_j] = \delta_{ij}$ and

$$\mathbf{A}_n = \mathbf{A}_1 + 2\zeta_\beta \omega_0 \Delta t^{2-\beta} \mathbf{A}_{2-\beta} + \omega_0^2 \Delta t^2 \mathbf{A}_2; \mathbf{B}_n = \mathbf{A}_2 \Delta t^2 \quad (7)$$

being \mathbf{A}_γ ($\gamma=1, 2-\beta, 2$) a lower bound strip matrix [2] whose first column elements are given as $A_{\gamma 1} = 1, A_{\gamma 2} = \gamma, A_{\gamma ij} = A_{\gamma i, j-1} (1 + \gamma_{j-2}) / (j-1)$ from eq. (5) we get

$$E[\mathbf{X}_n \mathbf{X}_n^T] = \mathbf{A}_n^{-1} \mathbf{B}_n \left[\Psi^{\frac{1}{2}} \mathbf{\Psi}_n^T \right] (\mathbf{B}_n^{-T} \mathbf{A}_n^T) \quad (8)$$

From this equation the entire correlation matrix of the response process is easily determined.

3. Concluding Remarks

The stochastic analysis of a structural system with fractional viscoelastic device is presented. The forcing function is modelled as a non-stationary white noise. Integrating the eq. motion by the Grünwald-Letnikov integration scheme returns easily the time dependent statistics of response process at the discretized times t_1, t_2, \dots, t_n .

References

- [1] NUTTING, P. G., *Journal of the Franklin Institute*, Maggio 1921.
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